## 天然裂缝性碳酸盐岩封闭油藏产量 递减规律研究及应用

姚 军 侯力群 李爱芬 石油大学(华东)

摘要:建立了天然裂缝性碳酸盐岩封闭油藏渗流模型。考虑了封闭油藏定井底压力和变井底压力两种不同的内边 界情形,并采用 Laplace 变换和 Duhamel 原理对数学模型进行了求解,得到了天然裂缝性碳酸盐岩封闭油藏的递减 曲线、在曲线上产量出现两个明显的递减阶段和两个相对平缓的递减阶段、讨论了审流系数和裂缝弹性储容比对 天然裂缝性油藏递减曲线的影响。实例表明,实际产量资料与理论递减曲线的拟合可确定地层参数,预测产量变

关键词:天然裂缝性油茂,产量遊滅规律,碳酸盐岩;渗流模型

中图分类号: TE344

文赵标识码:A

文章编号:1009-9603(2005)01-0056-03

### 引言

天然裂缝性油藏在我国油气资源中占有十分重 要的地位,由于裂缝性油藏的复杂性,对该类油藏的 产量进行预测难度较大。本文运用油气渗流力学理 论,建立了能够描述天然裂缝性油藏产量变化的渗 流数学模型,从理论上分析、阐述了天然裂缝性油藏 的产量变化特点和规律,为制定天然裂缝性油藏的 合理生产制度提供理论指导。

### 渗流物理模型

天然裂缝性碳酸盐岩封闭油藏是由基岩孔隙系 统和裂缝系统组成的连续介质[1]。相对于裂缝系 统而言基岩系统的导流能力很小,渗流物理模型中 只考虑裂缝系统向井筒供液,基岩系统的作用只是 向裂缝系统窜流[2]。为了建立物理模型须作如下 假设:①地层流体和地层岩石为微可压缩,流体为单 相流动,压缩系数为常数;②流体在基岩系统和裂缝 系统中的渗流满足达西渗流方程;③地层中仅一口 井,油井投产前地层中压力均匀分布;④忽略重力和 毛管力的影响;⑤忽略基岩内部的流体流动,基岩作 为供液源[3,4]。

## **渗流数学模型及其解**

#### 2.1 渗流数学模型

裂缝系统的渗流方程为

$$\frac{\partial^{2} p_{\text{fD}}}{\partial r_{\text{D}}^{2}} + \frac{1}{r_{\text{D}}} \cdot \frac{\partial p_{\text{fD}}}{\partial r_{\text{D}}} = (1 - \omega) \frac{\partial p_{\text{fD}}}{\partial t_{\text{D}}} + \omega \frac{\partial p_{\text{fD}}}{\partial t_{\text{D}}} (1)$$

基岩系统向裂缝系统的窜流方程为

$$(1 - \omega) \frac{\partial p_{mD}}{\partial t_{D}} = \lambda (p_{mD} - p_{mD})$$
 (2)

初始条件为

$$p_{\text{fD}}|_{t_{\text{D}}=0} = p_{\text{mD}}|_{t_{\text{D}}=0} = 0$$
 (3)

定井底压力下内边界条件为

$$p_{\text{fD}} - s \left( \frac{\partial p_{\text{fD}}}{\partial t_{\text{D}}} \right)_{r_{\text{D}} = 1} = 1 \tag{4}$$

变井底压力下内边界条件为

$$p_{\rm m} - s \left(\frac{\partial p_{\rm m}}{\partial t_{\rm D}}\right)_{r_{\rm D}=1} = p_{\rm wD}(t_{\rm D}) \tag{5}$$

封闭油藏的无因次外边界条件为

$$\left. \frac{\partial p_{\rm m}}{\partial r_{\rm D}} \right|_{r_{\rm D} = r_{\rm eD}} = 0 \tag{6}$$

无因次流量为[5]

$$q_{\rm D}(t_{\rm D}) = -\left(\frac{\partial p_{\rm D}}{\partial r_{\rm D}}\right)_{r_{\rm D}=1} \tag{7}$$

收稿日期 2004 - 10 - 14;改回日期 2004 - 12 - 20。

作者简介:姚军,男,教授,博士生导师,1984年毕业于华东石油学院采油工程专业,长期从事油气田开发工程的教学与科研工作。联系电 话:(0546)8392270,通讯地址:(257061)山东省东营市北二路271号石油大学(华东)石油工程学院。

式中:p 为压力,MPa;t 为时间,s;s 为表皮系数;r 为泄油半径,m;q 为产量, $m^3/d$ ;f 为裂缝系统;m 为基岩系统;w 为井底;e 为油藏外边界; $q_p$ 为无因次产量; $p_{jp}$ 为无因次压力(j=m,f); $t_p$ 为无因次时间; $\omega$  为裂缝系统弹性储容比; $\lambda$  为窜流系数。

#### 2.2 定井底压力条件下的产量公式

对于定井底压力数学模型,采用 Laplace 变换进行求解,得到定井底压力条件下 Laplace 空间无因次流量为

 $\bar{q}_{\mathrm{D}}(z) =$ 

$$\frac{M[K_{1}(M)I_{1}(r_{eD}M) - I_{1}(M)K_{1}(r_{eD}M)]}{sK_{1}(r_{eD}M)[I_{0}(M) - zMI_{1}(M)] + sI_{1}(r_{eD}M)[K_{0}(M) + zMK_{1}(M)]}$$

$$M = \sqrt{zf(z)} \tag{9}$$

式中: 为拉普拉斯算子;  $K_0(x)$  为零阶第二类虚宗量 Bessel 函数;  $K_1(x)$  为阶第二类虚宗量 Bessel 函数;  $I_0(x)$  为零阶第一类虚宗量 Bessel 函数;  $I_1(x)$  为阶第一类虚宗量 Bessel 函数。

#### 2.3 变井底压力条件下的产量公式

对于变井底压力数学模型, 也采用 Laplace 变换进行求解,得到变井底压力条件下无因次流量为 $q_{\mathrm{D}}(z)$  =

$$\frac{\bar{P}_{w}(z)M[K_{1}(M)I_{1}(r_{eD}M) - I_{1}(M)K_{1}(r_{eD}M)]}{K_{1}(r_{eD}M)[I_{0}(M) - zMI_{1}(M)] + I_{1}(r_{eD}M)[K_{0}(M) + zMK_{1}(M)]}$$
(10)

将式(8)和(10)进行数值 Laplace 反演可得到 真实空间中的无因次产量  $q_D$ 随无因次时间  $\iota_D$ 的变 化。

## 3 产量变化特征

对公式(8)或(10)采用数值 Laplace 反演计算可得到天然裂缝性油藏的产量。

#### 3.1 产量特征

均质油藏的产量有一个相对平缓的递减阶段和 迅速递减的阶段(压力波到达封闭边界后)。而天 然裂缝性油藏整个生产过程中产量出现两个相对平 缓稳定阶段和两个递减阶段(图1)。第一个平缓阶 段主要反映了裂缝系统的流动,持续时间较短;第一 个下降阶段主要反映了基岩往裂缝系统的窜流;第 二个平缓阶段表明基岩往裂缝流动和裂缝往井筒的 流动达到平衡,此时相当于一个均质系统,持续时间 远比第一个平缓阶段长;第二个产量递减阶段主要

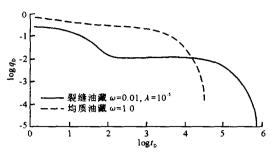


图 1 均质油藏与天然裂缝油藏的产量递减曲线

是受封闭外边界的影响,产量迅速下降。

### 3.2 影响产量递减曲线的参数

#### 3.2.1 窜流因子

裂缝系统的产量递减非常快。窜流因子越大, 第二个相对平级的递减阶段产量越高;窜流因子较 小时,第二个递减阶段的产量很小,几乎为零(图 2)。

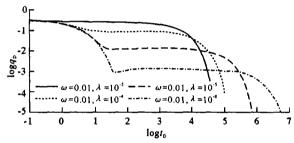


图 2 封闭定压下窜流因子对产量的影响

#### 3.2.2 裂缝弹性储容比

裂缝弹性储容比越大,裂缝系统的弹性能量越大;裂缝系统流体流动时间越长,第一个平缓阶段持续时间越长(图3)。

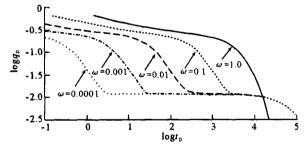


图 3 裂缝弹性储容比对天然裂缝性 油藏产量递减曲线的影响

#### 3.2.3 变井底压力

天然裂缝性封闭油藏在变井底压力下的双对数 生产曲线与定井底压力条件下的递减曲线一样,都 有两个拐点,第一个拐点体现了基岩系统向裂缝系 统发生拟稳态窜流的开始,第二个拐点体现了窜流 过程的结束,两个系统的压力达到了平衡,可视为一 个均质系统的情况(图4)。对比天然裂缝性封闭油 藏定井底压力和变井底压力的双对数递减曲线(图5)。曲线的前部分(即第一拐点前)变井底压力和定井底压力的曲线几乎重合,这是因为基岩和裂缝通过窜流达到压力平衡的时间期较短,压力降不明显。当窜流结束两个系统的压力平衡后,变井底压力条件下的产量下降的速度大于定井底压力条件下的速度,递减加快。

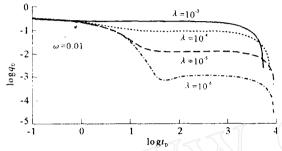


图 4 封闭油藏变并底压下的双对数生产曲线

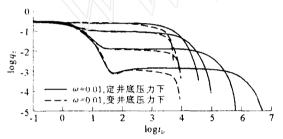


图 5 封闭油藏不同内边界下的双对数对比曲线

## 4 矿场应用

塔河油田奧陶系油藏是以裂缝、溶洞发育为主的碳酸盐岩油藏,可分为裂缝发育型和溶洞发育型。从裂缝型油藏某井的实际生产数据与天然裂缝性油藏的理论递减曲线的拟合图(图6)可以看出,该井的实际生产数据与天然裂缝性油藏的理论递减曲线的特征拟合较好,通过拟合得到主要地层参数:裂缝

弹性储容比为  $2.8 \times 10^{-2}$ ; 裂缝系统的渗透率  $761 \times 10^{-3} \mu m^2$ ; 污染系数为 0.5; 窜流系数为  $3.2 \times 10^{-5}$ ; 封闭边界半径为 193.0 m。

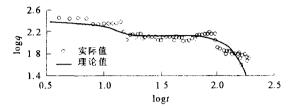


图 6 某油井实际生产数据与理论计算数据拟合图

## 5 结论

天然裂發性油藏的产量双对数曲线上有两个相 对平缓的递减阶段和两个迅速递减阶段;裂缝系统 的产量递减较快;窜流因子越大,第二个相对平缓的 递减阶段产量越高;裂缝弹性储容比越大,裂缝系统 流体流动时间越长。

通过实际生产资料与理论计算产量递减曲线的 拟合,可以确定地层也可以预测今后的产量。

#### 参考文献:

- 1 Prat G D. Well test analysis for naturally fractured reservoir; [Ph. D. Thesis]. Stanford: Stanford University, 1980
- Warren J E , Root P J. The behavior of naturally fractured reservoirs. SPE 426
- 3 姚军,戴卫华,王子胜等.变井简储存的三重介质油藏试井解释方法研究.石油大学学报(自然科学版),2004,28(2):46~51
- 4 Olarewaju J S, Schlumberger Dawell, Lee W J. Rate behavior of dual porosity reservoir. SPE 21703
- 5 Everdingen Van, Hurst W. The application of the Laplace transformation to flow problems in reservoirs. Trans, AIME, 1949, 186(12):305 ~324

编辑 刘北羿

欢迎报稿 欢迎订阅

Cui Wenfu. Classification of intercalation and the longitudinal remaining oil distribution pattern in reverse rhythm thick reservoir-taking  $8 \sim 15$  sand bodies of Es<sub>2</sub> in Shengtuo oilfield as examples. *PGRE*, 2005, 12(1):  $52 \sim 55$ 

Characteristics of intercalation distribution in reverse rhythm thick reservoir of delta front were studied systematically in 8 ~ 15 sand bodies of Es<sub>2</sub> in Shengtuo oilfield. The intercalation is divided into 54 kinds of combination. And then four kinds of shield formed by oil and water migration for different combinations were analyzed. By applying different field data, seven distribution patterns for longitudinal remaining oil of this kind of reservoirs at the extra high water-cut stage were studied, and then corresponding measures for tapping the potential were worked out, which is of great value in the adjustment and further development of Shengtuo oilfield.

Key words: delta front, thick reservoir, intercalation, remaining oil, pattern

Cui Wenfu, Shengli Oil Production Plant, Shengli oil-field Ltd. Co., Dongying City, Shandong Province, 257051, China

## Yao Jun, Hou Liqun, Li Aifen. Research and application on production decline rule of closed carbonate reservoir with natural fractures. PGRE, 2005, 12(1): $56 \sim 58$

A percolation model for closed carbonate reservoir with natural fractures was built. Considering both constant and variable bottomhole pressure as the inner boundary conditions and solving its corresponding mathematical model using Laplace transform and Duhamel principle gave decline curve of the production rate in the oil reservoir, on which both two rapid declining phases and two relative gentle ones appeared. The influence of interporosity flow coefficient and elastic storage -volume ratio on the decline curve for the naturally fractured reservoir was discussed. Field example demonstrates that by matching actual production data with theoretical decline curve formation parameters can be determined and future production can be predicted.

Key words: naturally fractured reservoir, production decline rule, carbonate rock, percolation model

Yao Jun, Petroleum Engineering Institute, University of Petroleum, Dongying City, Shandong Province, 257061, China

## Sun Jianping, Ran Qiquan, Shi Huandian. Water-flooding characteristic and effect evaluation of the fractured volcanic heavy oil reservoir of block Zao35. *PGRE*, 2005, 12(1): 59 ~ 62

According to the characteristics of fracture distribution and fluid in the fractured volcanic oil reservoir of block Zao35, dynamic data after water flooding were analyzed in detail using reservoir engineering method. After waterflood development in this oil reservoir, the trend of sudden drop in formation pressure was controlled and began to rise slowly, but the decline rate of the oil production was still very high. The injected water channeled rapidly along the natural fracture of this reservoir, and mest of the oil production wells were flooded severely. The water cut of this reservoir went up integrally and rapidly, and only after 15 months of waterinjection it entered high-water-cut period. Invalid cycle of the injected water made water-restrained rate, waterflooding index and volumetric sweep efficiency were very low. Water injection of 1 × 10<sup>4</sup> m<sup>3</sup> can only produce 0. 22 × 10<sup>4</sup> t equivalent oil. At present recovery percent of reserves is 4.06%, and the terminal recovery efficiency of water-flooding is less than 6%. Remaining recoverable reserve of the water-flooding reservoir was low, but the actual remaining recoverable reserve was high, so the potential of the oil reservoir can not be tapped efficiently. Other production way should be adopted to improve the usage degree of the remaining resources in this oil reservoir.

Key words: fracture, volcanic rock, heavy oil, water-flooding, effect evaluation, block Zao35

**Sun Jianping**, The Southwest Petroleum Institute, Chengdu City, Sichuan Province, 610500, China

# Yin Wenjun, Chen Yongsheng, Wang Hua et al. Building of the interpretation model of the large channels and remaining oil saturation by hydraulic survey. PGRE, 2005, 12(1): 63 ~ 65

The hydraulic survey technology is a well test one for surveying reservoir conditions between water injection wells and oil production wells. It can not only provide information of reasonable productivity, formation parameters, formation pressure and so on, but also apply in planar remaining oil survey in oil-bearing formations and the large channel recognition in development phase of extra high water cut. The interpretation model built by hydraulic survey of connected well-pair permeabili-